INFORMATIONAL HANDOUT FOR CONTRACTOR

Water Quality Information Handout

Replacement Planting and Irrigation

Contract No. 04-2G3624

04-ALA-92-PM R5.1/R5.8

California Department of Transportation District 04 Office of Water Quality 111 Grand Avenue, Oakland, CA 94612

November 1, 2013

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- 1. Vicinity Map
- 2. Rainfall Data
- 3. Construction Risk Level
 - Sediment Risk Factor Worksheet & Receiving Water Risk
 - Email (temporary fiber rolls to be remained permanent)

Disclaimer:

The non-storm water information handout is a guideline and is to be used for informational purposes only. It is not a waiver of the provisions in the National Pollutant Discharge Elimination System (NPDES) Construction General Permit (CGP), Number CAS 000002, adopted on September 2, 2009. Bidders and Contractors are to make all necessary investigations and examinations to satisfy conditions encountered to perform work and to conform to the requirements of the contract documents and the CGP.

1. Project Information

1A. Project Description

This project will replace the planting and irrigation on State Route 12 in Alameda from post mile 5.1 to 5.8. Construction is anticipated to span four months (120 days) and will include a plant establishment period of three years.

Latitude and Longitude:	<u>37.631920 -122.110680</u>
Construction Start Date	<u>06/01/2014</u>
Construction End Date	12/01/2017
Project Area	<u>12 ac</u>
Disturbed Soil Area	5.73 ac

1B. Receiving Water Bodies

The project's watershed is San Lorenzo Creek-Frontal San Francisco Bay Estuaries, the receiving water, with Ward Creek as a subwatershed, is on the 2010 303(d). Although the Risk Level map depicts the area as high risk for receiving water, San Lorenzo Creek is approximately 3.5 north, flows from the project area likely drain to San Francisco Bay (Lower), the receiving water can be changed from high risk to low risk, thus lowering the project risk level from 2 to 1. San Francisco Bay (Lower) is on the 2010 303(d) of Water Quality Limited Segments for Chlorande, Dieldrin, Dioxin Compounds, Furan Compounds, Invasive Species, Lead (sediment), Mercury (sediment), PAHs (Polycyclic Aromtic Hydrocarbons (sediment), Pestcides (sediment), and Zinc (sediment).

1C. Climate and Rainfall Data

A National Oceanic and Atmospheric Administration (NOAA) weather station located in Oakland, CA was used to obtain an estimated number of rainy days per year and qualifying rain events. The Compliance Storm Event was also downloaded from the NOAA website.

Rainy days per year (precipitation 0.10 inches or greater)	<u>33.2</u>	_days
Qualifying rain events per year	<u>11.1</u>	_days
Compliance Storm Event (rainfall total for the 5 year, 24 hr storm)	2.25	_inches

2. Construction General Permit

A Storm Water Pollution Prevention Plan is required since the disturbed soil area is 5.73 acres.

2A. Risk Level

R factor	<u>193.44</u>
K factor	<u>0.31</u>
LS factor	<u>0.16</u>
Sediment Risk	9.59

Receiving Water Body Risk	_ Yes/ High
Risk Level	1*

*The risk level was downgraded to risk level 1 from risk level 2. See attachment 3.

3. Temporary Construction Site BMPs

The estimated quantities of temporary construction site BMPs are in the PSE package. Temporary Fiber Rolls to remain permanent.

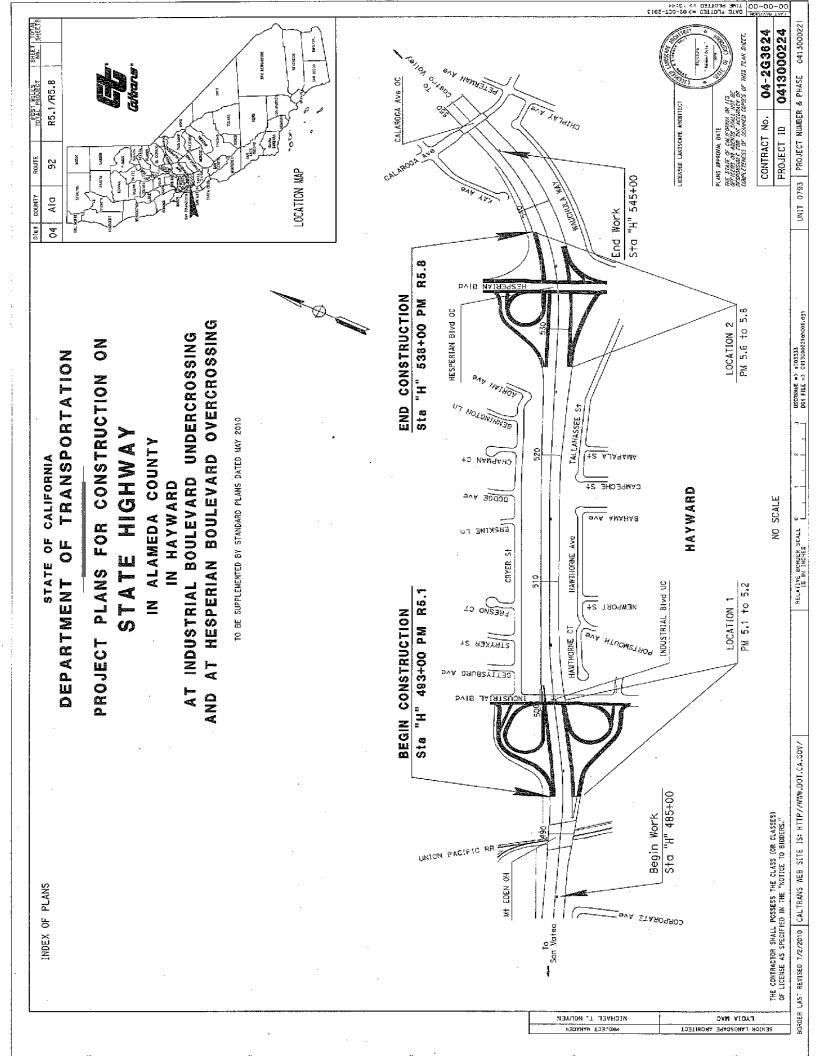
3A. Run-on Discharges

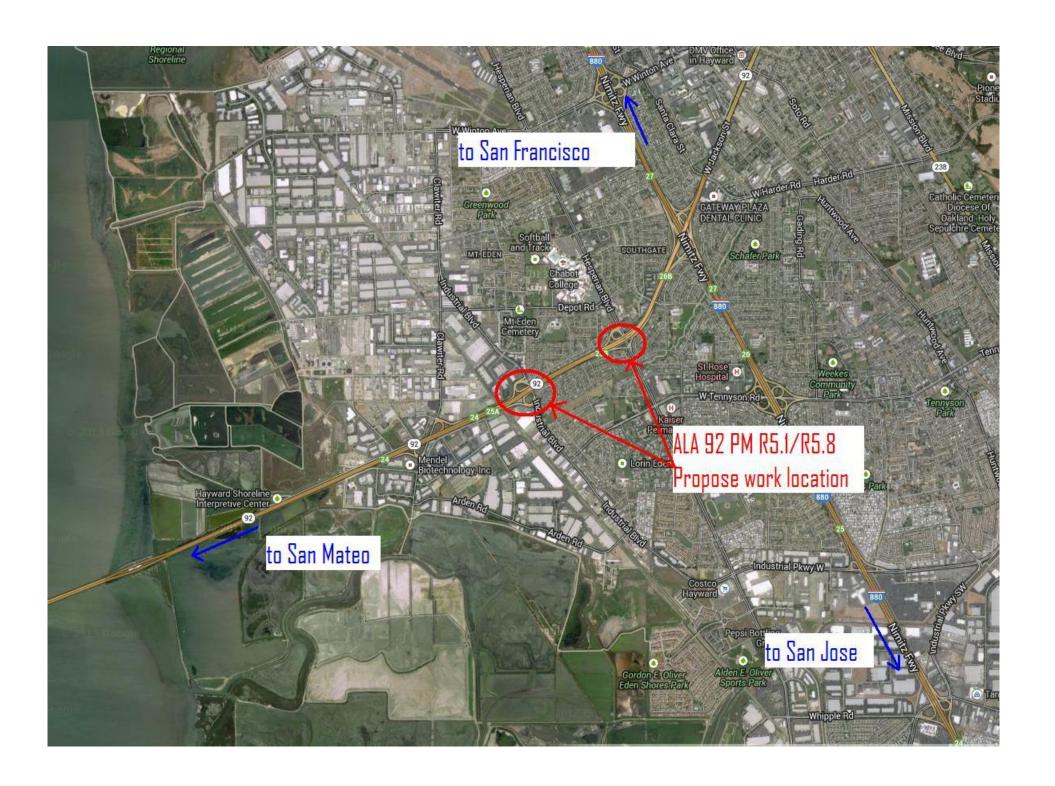
Run-on discharges are off-site storm water that can potentially run to the site. Run-on discharges should be calculated based on a rainfall intensity for a 2-year 24-hour event per the PPDG. The Rational Method is typically used to calculate run-on discharges.

Equation: Q=CiA where Q = Run-on discharge (cubic feet per second) C = Runoff coefficient (see HDM Figure 819.2A) i = 2-year, 24-hour rainfall intensity (inches/hour)

Note: Run-on is anticipated to be minimal; the Contractor needs to verify all run-on for the proposed project.

ATTACHMENT 1 VICINITY MAP





ATTACHMENT 2 RAINFALL DATA

Rainfall Intensity Information: http://www.wrcc.dri.edu/pcpnfreq/nca5y24.gif RAINNY DAYS PER YEAR & QUALIFYING RAIN EVENT PER YEAR

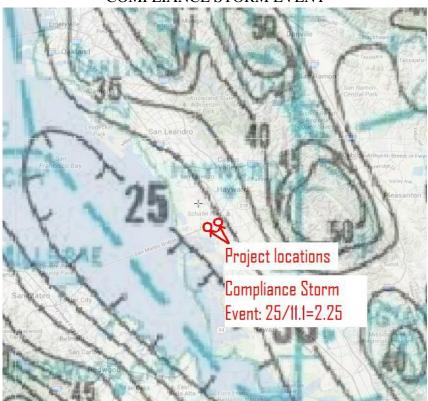
OAKLAND WSO AP

Elevation: 6 feet Start Year: 1948 End Year: 1985 Number of Years: 36

Average number of days per month with precipitation:

Month	>=0.1 in	>=0.5 in
January	6.2	2.4
February	5.2	1.9
March	5	1.4
April	2.7	0.7
May	1	0.1
June	0.3	0.1
July	0.1	0
August	0.2	0
September	0.4	0.1
October	1.7	0.6
November	4.6	1.6
December	5.8	2.1
Yearly Total	33.2	11.1

COMPLIANCE STORM EVENT



ATTACHMENT 3 CONSTRUCTION RISK LEVEL

Analyses of data indicated that when factors other than rainfall are held constant, soil loss is directly proportional to a rainfall factor composed of total storm kinetic energy (E) times the maximum 30-min intensity (I30) (Wischmeier and Smith, 1958). The numerical value of R is the average annual sum of El30 for storm events during a rainfall record of at least 22 years. "Isoerodent" maps were developed based on R values calculated for more than 1000 locations in the Western U.S. Refer to the link below to determine the R factor for the project site.

http://cfpub.epa.gov/npdes/stormwater/LEW/lewCalculator.cfm

R Factor Value 193.44

B) K Factor (weighted average, by area, for all site soils)

The soil-erodibility factor K represents: (1) susceptibility of soil or surface material to erosion, (2) transportability of the sediment, and (3) the amount and rate of runoff given a particular rainfall input, as measured under a standard condition. Fine-textured soils that are high in clay have low K values (about 0.05 to 0.15) because the particles are resistant to detachment. Coarse-textured soils, such as sandy soils, also have low K values (about 0.05 to 0.2) because of high infiltration resulting in low runoff even though these particles are easily detached. Medium-textured soils, such as a silt loam, have moderate K values (about 0.25 to 0.45) because they are moderately susceptible to particle detachment and they produce runoff at moderate rates. Soils having a high silt content are especially susceptible to erosion and have high K values, which can exceed 0.45 and can be as large as 0.65. Silt-size particles are easily detached and tend to crust, producing high rates and large volumes of runoff. Use Site-specific data must be submitted.

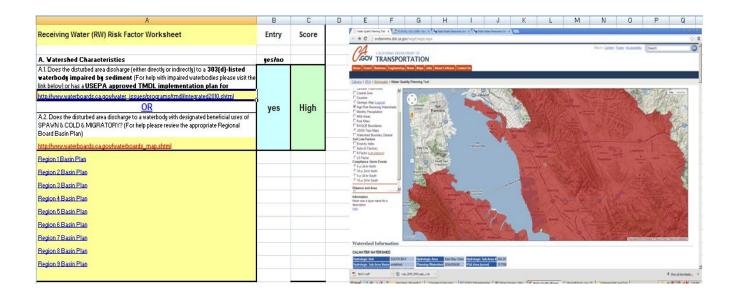
Site-specific K factor guidance

0.31 K Factor Value

C) LS Factor (weighted average, by area, for all slopes)

The effect of topography on erosion is accounted for by the LS factor, which combines the effects of a hillslopelength factor, L, and a hillslope-gradient factor, S. Generally speaking, as hillslope length and/or hillslope gradient increase, soil loss increases. As hillslope length increases, total soil loss and soil loss per unit area increase due to the progressive accumulation of runoff in the downslope direction. As the hillslope gradient increases, the velocity and erosivity of runoff increases. Use the LS table located in separate tab of this spreadsheet to determine LS factors. Estimate the weighted LS for the site prior to construction.

Table Table	
LS Factor Value	
Watershed Erosion Estimate (=RxKxL\$) in tons/acre	9.594624
Site Sediment Risk Factor	
Low Sediment Risk: < 15 tons/acre	
Medium Sediment Risk: >=15 and <75 tons/acre	Low
High Sediment Risk: >= 75 tons/acre	



EA 2G362, 04-ALA-92 PM 5.1/5.8

Trang Hoang, 8/28/2013

The project's watershed is San Lorenzo Creek-Frontal SF Bay Est, with Ward Creek as a subwatershed. Although the RL map depicts the area as high risk for receiving water, San Lorenzo Creek is approx 3.5 north and flows from the project area drains to SF bay (lower), which is not impaired for sediment nor has the beneficial uses of COLD, MIGR, or SPWN. The receiving waters can be changed from high risk to low, thus lowering the project's risk level from 2 to 1.

This was approved by Kamran Nakhjiri, Water Pollution Control Senior.

